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DIRECT-DRIVE ARCHITECTURE FOR SOLAR ELECTRIC PROPULSION

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1 - INTRODUCTION

/// Solar System exploration requires high power electric propulsion to move heavy payload over long distance

/// Power systems will have to generate and distribute several tens of kW

- /// For inner planet of solar system, current approach is to use 100V solar array, MPPT converter and PPU with converter
- *I* Mass, cost and dissipation will become more and more difficult to handle with power increase
- /// « Direct-Drive » for Solar Electric Propulsion intends to remove every converter between solar array and electric thruster
- I Less dissipation, more power available, less mass and cost
- I Direct drive is a virtuous circle, mandatory for Deep Space Exploration using SEP

/// The Horizon 2020 project «European Direct-Drive Architecture » gathers a consortium that will study, manufacture and test a large representative mockup.

Universidad

Carlos II







2 - SOLAR ELECTRIC PROPULSION IN SOLAR SYSTEM

/// Solar flux decreases quickly with sun distance

/// Beyond the asteroïd belt, using solar array to power high power electric propulsion is **not reasonable**

/// Past / current missions using SEP as main propulsion

- Deep Space 1 : Asteroïd / 2.3kW
- Hayabusa 1: Asteroïd / 350W
- Smart 1: Moon / 1.4kW
- Dawn: Vesta & Ceres / 2.5kW
- Hayabusa 2: Asteroïd / 420W
- BepiColombo: Mercury / 11kW

/// Future missions

- Power and Propulsion Element (PPE): Moon / ~25kW
- Psyche: Asteroïd / 4.5kW
- DART: Asteroïd / 7.5kW
- Mars Sample Return (Earth Return Orbiter) : Mars / ~30kW
- Asteroïd Retrieval Robotic Mission (cancelled) : Asteroïd / ~30-50kW

/// More and more missions to come using several tens of kW





3 - CURRENT ELECTRICAL ARCHITECTURE



3 - CURRENT ELECTRICAL ARCHITECTURE

/// Example BepiColombo MTM (Mercury Transfer Module)

- / Solar Array > 100V near earth (and at each eclipse exit) and down to 42V near Mercury
- Power conditioning used as shunt when MPP voltage is >100V and as boost when MPP voltage is < 100V</p>
- 100V « sun regulated » main power bus
- No battery discharge regulator
- I PPU are supplied through unprotected LCL (10A)
- 28V secondary bus

More information on: **BepiColombo MTM Power Conditioning And Distribution Unit**, *Hansen Magnus Moberg*, presented at 9th ESPC (European Space Power Conference), 2011, Saint-Raphaël, France



4 - DIRECT DRIVE ARCHITECTURE

/// Description

- I « Direct » connection of solar array with thruster anode
- Removal of PPU anode converter module, and increase of bus voltage until anode operating voltage (300V-500V for Hall Effect Thrusters and 300V-1000V for HEMPT)
- Past studies have shown feasibility of SA voltage and regulation at 300V and above

/// Interests

- Increased efficiency
- Less volume and cost
- I Decreased thermal dissipation.

/// Drawbacks

- Primary bus voltage must fit thruster voltage.
- Modification of thruster operating

point has a direct impact on the bus voltage.

- No isolation between thruster and bus.
 - Need of Cathode Reference Potential (CRP) bias supply



/// 7



Loads

Low power units

4 - DIRECT DRIVE ARCHITECTURE

/// Focus on « MPPT » technique without power/voltage conversion

- / On interplanetary missions, solar array temperature is subject to large variation as sun distance is evolving
- *I* Maximum Power Point Tracking is <u>mandatory</u> but various technique exist
- I Most commonly used technique is to use an high efficient (95 to 96%) buck or boost power converter, and a MPPT algorithm which track the voltage of solar array MPP and apply this voltage at solar array input.

« Direct-drive » would not be complete if this power converter remains between solar array and thrusters

/// Principle of MPPT without conversion

- 2 solutions
- Adaptation of the load current to equalize it with current of maximum power point of the solar array
 - Thruster can adapt its Xenon flow rate to modify the requested current.
- Using a battery and its charge/discharge converter (BCDR) to adjust in real time a voltage on the bus corresponding to the voltage of maximum power point (Vmp) of solar array
- S3R cells are used in PCDU, leading to high efficiency of transfer (99%)



4 - DIRECT DRIVE ARCHITECTURE

/// Each electric thruster has its own « performance map » giving its limits in term of voltage and current

/// SA characteristic is always within the thruster performance map for a Earth-Mars mission

/// If it is not possible to keep SA MPP within performance map (too much variation of solar flux and temperature)

- Possibility to tilt the SA to reduce extremes values
 - Highly recommanded for missions to Mercury or closer to Sun to limit SA temperature
- In table below: several examples of 100m²/30kW (@1AU) solar array designed to stay within 300V-400V range (with different serie – parallel layout, but same surface)



					1
	Vmp at Earth	Max Power at Earth	Vmp at targeted	Max Power at	SA
			body	targeted body	Layout
Earth-Ceres	300V (SA tilt =	17.5kW (SA tilt = 60°)	365V (SA tilt= 0°)	4.8kW (SA tilt= 0°)	100s300p
	60°)				
Earth-Mars	300V (SA tilt= 0°)	30kW (SA tilt= 0°)	383V (SA tilt= 0°)	13.5kW (SA tilt= 0°)	120s250p
Earth-Moon	300V (SA tilt= 0°)	30kW (SA tilt= 0°)	300V (SA tilt= 0°)	30kW (SA tilt= 0°)	120s250p
Earth-Venus	365V (SA tilt= 0°)	30kW (SA tilt= 0°)	310V (SA tilt= 0°)	49.8kW (SA tilt= 0°)	146s205p
Earth-	488V (SA tilt= 0°)	30kW (SA tilt= 0°)	300V (SA tilt=	60.8kW (SA tilt=	195s154p
Mercury	But SA exploited	But only 26.1kW	70°)	70°)	
	at 400V max	extracted at 400V			

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5 - STATE-OF-THE-ART OF DIRECT DRIVE ARCHITECTURE

/// State-of-the-art

- Studies have been done by NASA in the 70's but abandoned since only GIE was the use case: Bus voltage was too high (>1000V)
- I In the 90's, with advent of HET, NASA has made new studies and breadboard
 - D2HET (Direct Drive Hall Effect Thruster)
 - National Direct-Drive testbed
- SITAEL also conducted a certain number of studies and thesis at EP subsystem level
- I Thales Alenia Space conducted a H2020 in 2016-2017 to prove the feasibility of a high voltage bus (300V to 600V)
- High-Voltage Electrical Power System Architecture: <u>http://hv-epsa-h2020.eu/</u>





6 - EUROPEAN DIRECT-DRIVE ARCHITECTURE (EDDA)

/// Work to be performed within H2020 EDDA

- I Objectives of the project
 - 1. Increase PPU efficiency from 95% to 99%
 - 2. Enable MPPT without power conversion
- 3. Reduce by half PPU mass and cost



- 4. Having same direct-drive architecture for both Hall Effect Thrusters (HET) and High Efficiency Multistage Plasma Thruster (HEMPT).
- 5. Increase TRL from TRL2 to TRL4 or 5
- / Website of the project: https://edda-h2020.eu/
- I Description of the mockup
- A High voltage Solar Array Simulator able to reproduce SA behavior in flight
- A battery simulator, using a DC/DC bidirectional power supply
- A PCU, including
 - Representative S3R; BCDR (Battery charge and discharge regulator); Bus capacitance; Switches; Control unit (with dSpace)
- Loads, with simple power resistors and input switch

- Direct-Drive Unit, including
 - · CRP bias supply ; Filter unit ; Auxiliary supplies
- Gas supply, including
 - Gas tank ; Valve (provided by thruster manufacturers)
- Thrusters (provided by thruster manufacturers)
 - 2 x HT5k magnetically shielded from Sitael
 - 1 x HEMPT 30250 from Thales Deutschland



6 - EUROPEAN DIRECT-DRIVE ARCHITECTURE (EDDA)



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CONCLUSION

/// Direct-Drive is mandatory for high power Solar Electric Propulsion

- /// Although restricted to 300V-class thruster (HET and HEMPT), the concept is fully applicable to higher voltage thruster (Gridded Ion Engine > 1000V)
- *I* Current state of technology do not allow to produce and distribute power at this voltage using solar arrays.
- Although GIE are commonly used for deep space exploration (higher lsp), very high power electric propulsion (20kWclass thrusters, or more) will make use of HET or HEMPT which are less complex, in particular for this class of power
- I The use of direct-drive increase the efficiency of the overall propulsion system
- /// The H2020 EDDA project will allow to test a representative mockup for 5kW class thrusters. Conclusion of the study will be applicable to 20kW-class thrusters and beyond.









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